



Development of resilient response and damage models for HMA.

Prepared for presentation at the 18th RPF Pretoria, November 2009 By: Erik Denneman

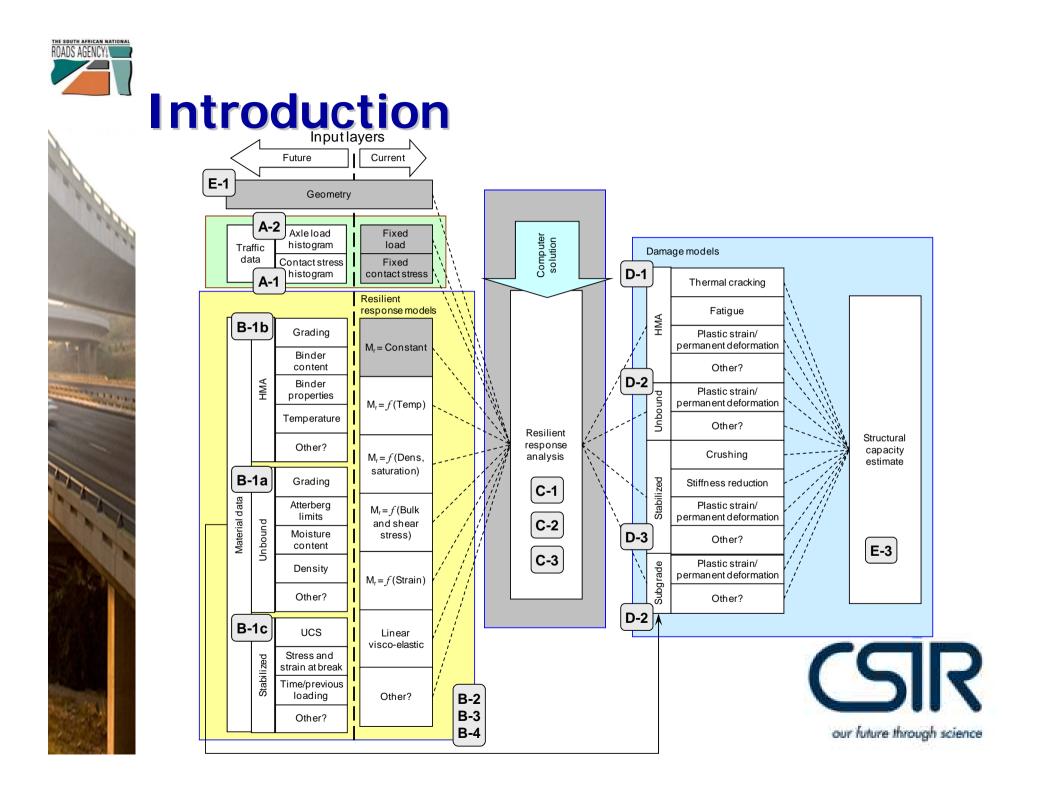




Presentation structure

- Introduction,
- State of the art in M-E design of HMA and the availability of models for SAn practise,
- Components of the envisaged design method,
- Structure of laboratory test program,
- Test results: by Dr. Joseph Anochie- Boateng







State of the art in HMA design

Three components:

- Environment,
 - Traffic load, speed, temperature.
- Resilient response,
 - Complex modulus as a function of age, density, grading, binder type, frequency, etc.
- Damage models,
 - Rutting: as a function of stiffness, or based on repeated load test,
 - Fatigue: as a function of stiffness, or based on beam test results.





Current HMA design models

HMA design in South Africa mostly based on reactive specifications.

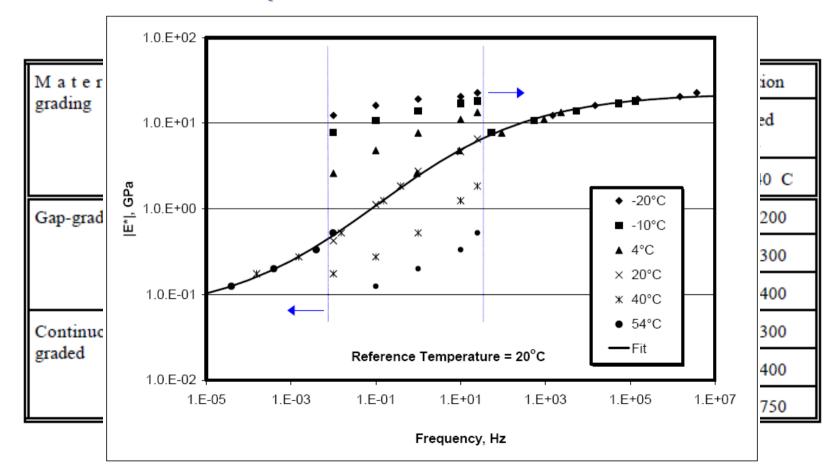
ME design:

- Environment:
 - Load: E80s, loading time (10Hz), average temperature
- Resilient response
 - Default values
- Damage models
 - No rutting model,
 - One size fits all fatigue relation





Resilient response:

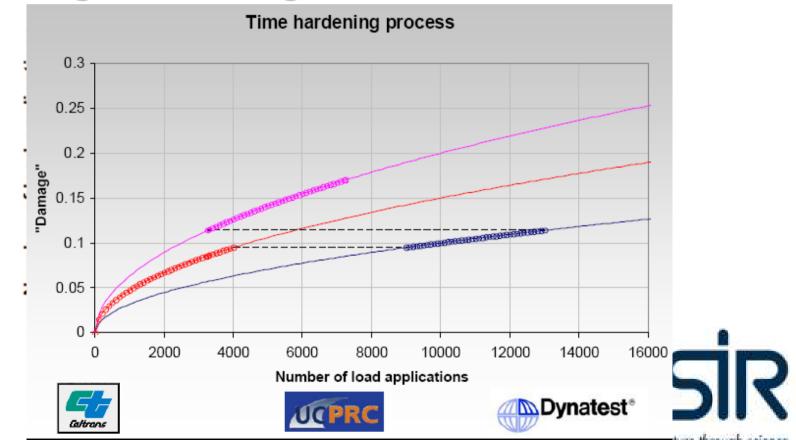


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Fatigue & Rutting

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Envisaged M-E design for HMA

- Different levels of analysis depending on client requirements and risk.
 - Level 1: Full material characterization,
 - Level 2: Some material characterization,
 - Level 3: Use of default values
 - Level 1:
 - G* binder characterization,
 - Complex modulus frequency sweep on mix,
 - Repeated load testing for fatigue and rutting,
 - Modelling based on full set of results.



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Envisaged M-E design for HMA

- Level 2 (tentative):
 - G* binder characterization,
 - Complex modulus frequency sweep on mix,
 - Use of stiffness values to model rutting/fatigue damage
- Level 3:
 - Use default values for G* binder,
 - Predict complex modulus for mix (Witczak, Hirsch type relation)
 - Use of predicted stiffness values to model rutting/fatigue damage





Dynamic Modulus

20		
$\log \left E^* \right = 3.750063 + 0.02932 P_{200} - 0.001767 (P_{200})^2 + 0.002841 P_4 - 0.058097 V_a$		
0.000000	V_{beff} [3	$\frac{1.871977 - 0.0021P_4 + 0.003958P_{38} - 0.000017(P_{38})^2 + 0.005470P_{34}}{1 + e^{(-0.603313 - 0.313351\log f - 0.393532\log \eta)}}$
- 0.802208	$\left(V_{beff} + V_a\right)^+$	$1 + e^{(-0.603313 - 0.313351\log f - 0.393532\log \eta)}$
State of Sta		
The second	E*	= asphalt mix complex modulus, in 10^5 psi (145 psi = 1 MPa);
COMPANY OF THE OWNER OF THE OWNER	η	= binder viscosity, in 10 ⁶ poise [10 Poise = 1 pa.s];
	f	= load frequency, in Hz;
	Va	= % air voids in the mix, by volume;
2	V _{beff}	= % effective bitumen content, by volume;
	P ₃₄	= % retained on $\frac{3}{4}$ -in. [19.0-mm]
A A A	P ₃₈	= % retained on 3/8-in. [9.5-mm]
	P ₄	= % retained on No. 4 [4.75-mm]
	P ₂₀₀	= % passing No. 200 [0.075-mm]





HMA research effort

- Selection/development of appropriate test protocols,
- Laboratory testing,
 - Model development,
- Field validation.





Laboratory test program

5 (+1) mixes:

- 1. BTB, 40/50 pen binder,
- 2. Coarse continuous, AE2 binder,
- 3. Medium continuous, AE2 binder,
- 4. Bitumen rubber,
- 5. Medium continuous, 60/70 binder,
- 6. (+HiMA)
- Progress:
 - Mix 1 testing completed,
 - Mix 2 & 3 in progress





Sample Preparation:

Binder testing:

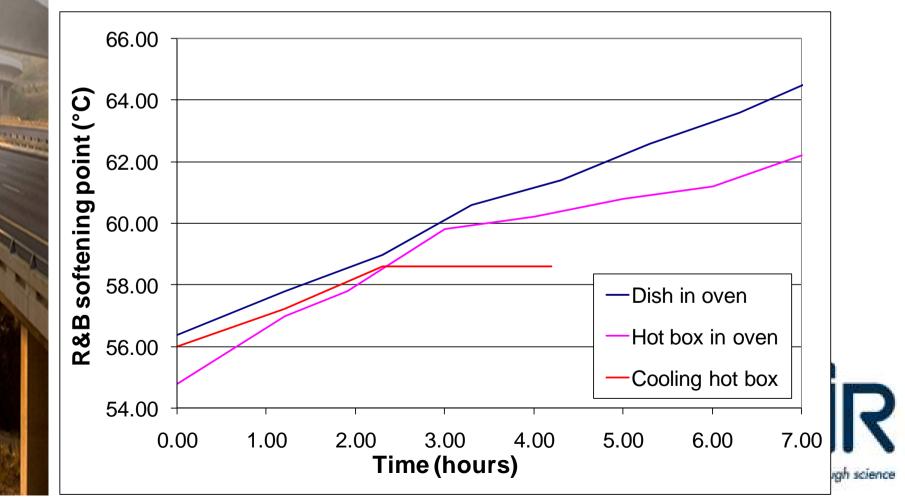
- Binder sourced at the plant => RTFOT, PAV
- Binder recovered, from the field (aging),
- Binder recovered from laboratory samples.
- HMA mix preparation:
 - Initial plan: compact plant produced mix,
 - Revised plan: Produce mix from components,
 - Conditioning of samples:
 - Short term aging to simulate production aging,
 - Long term aging to simulate 5-10 years inservice aging.





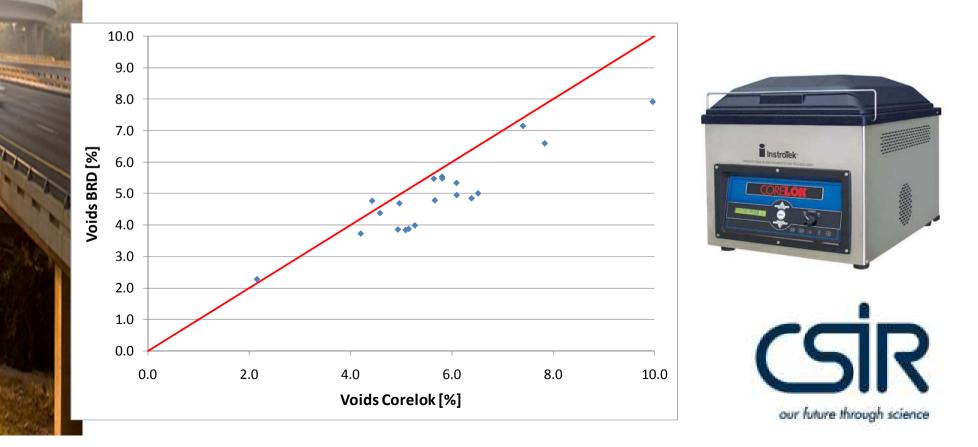
Sample Preparation:

Binder aging in hot-box





Conventional BRD vs Corelok





Summary

Process is on schedule,

- International best practise adapted for local conditions,
- The models will allow different levels of assessment,
- Method will be as simple as possible, but no simpler than that.

