

# SANRAL: Simulation of Vehicle Dynamics

Wynand JvdM Steyn



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1908 - 2008



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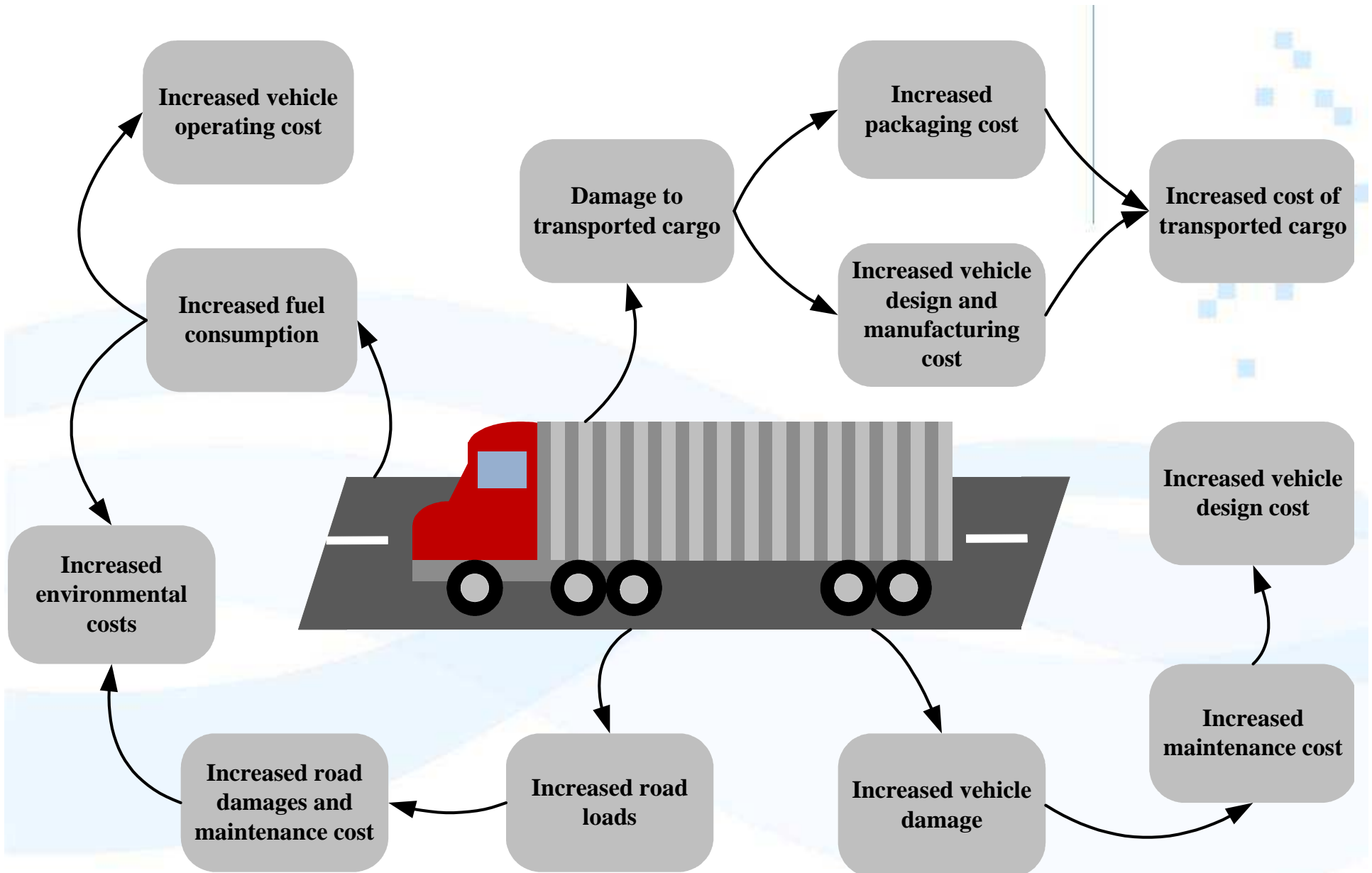
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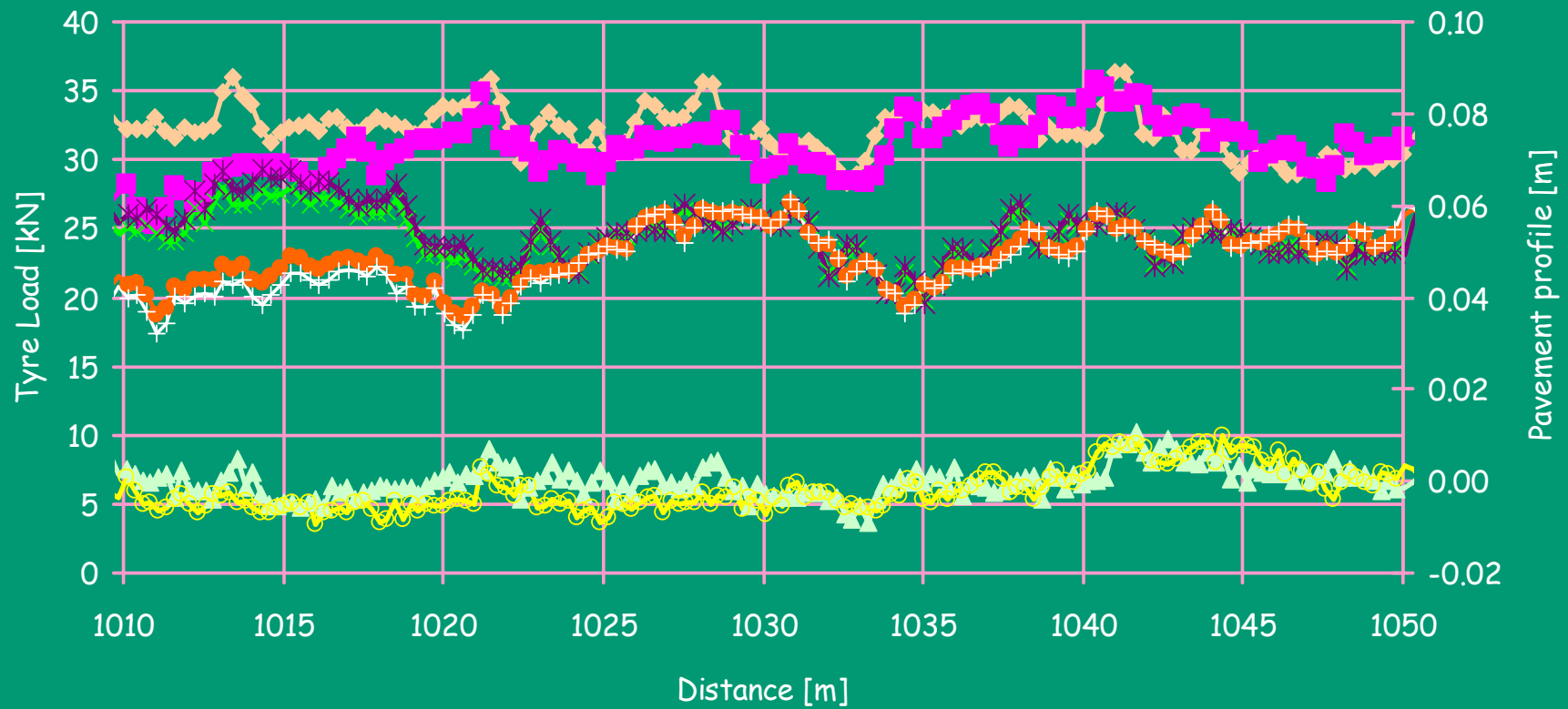
# What is the problem

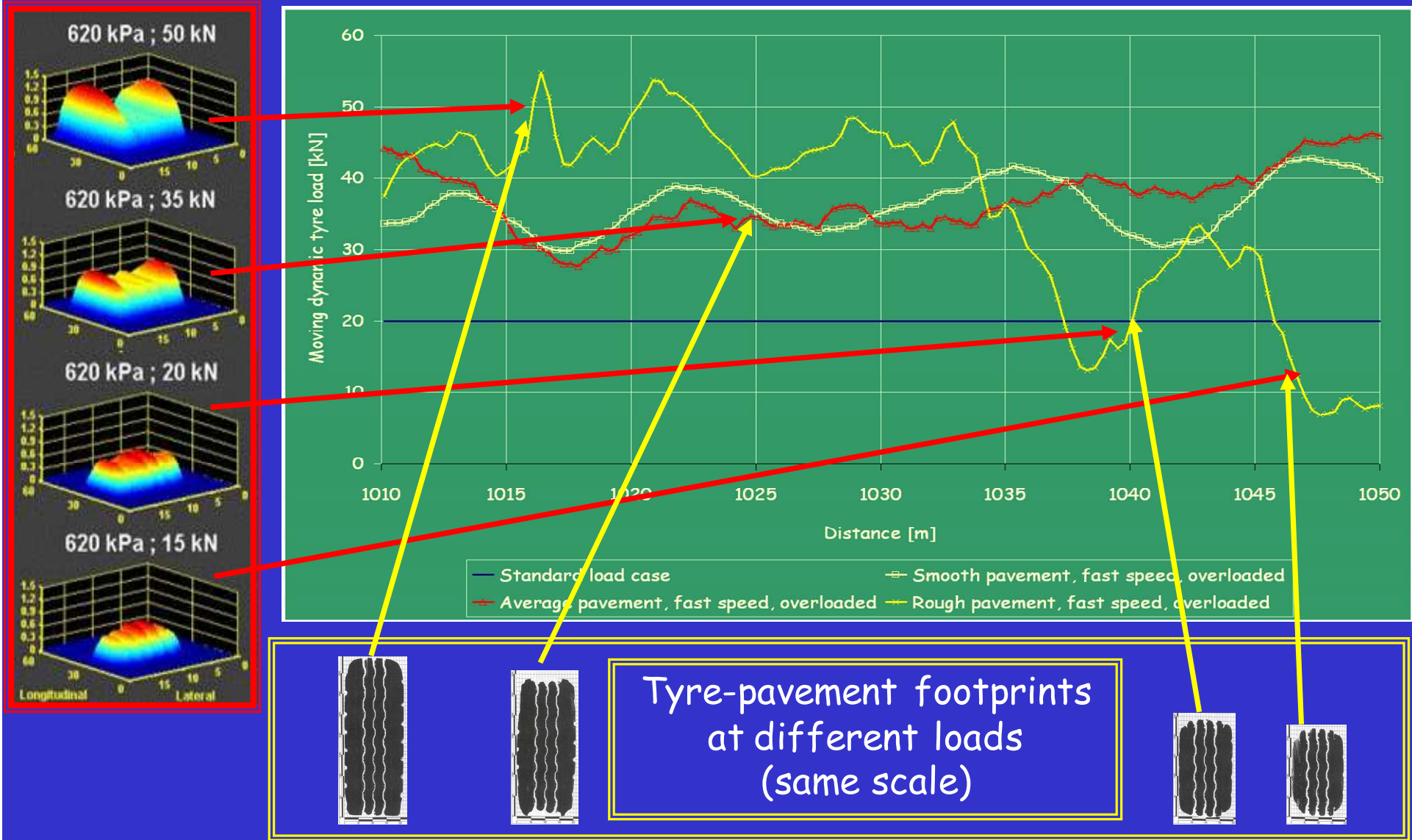
- Roads are not flat
- Uneven roads cause Moving Dynamic Loads (MDL)
- MDL cause range of loads on roads
- What do we design for?

# SANRAL project focus & background

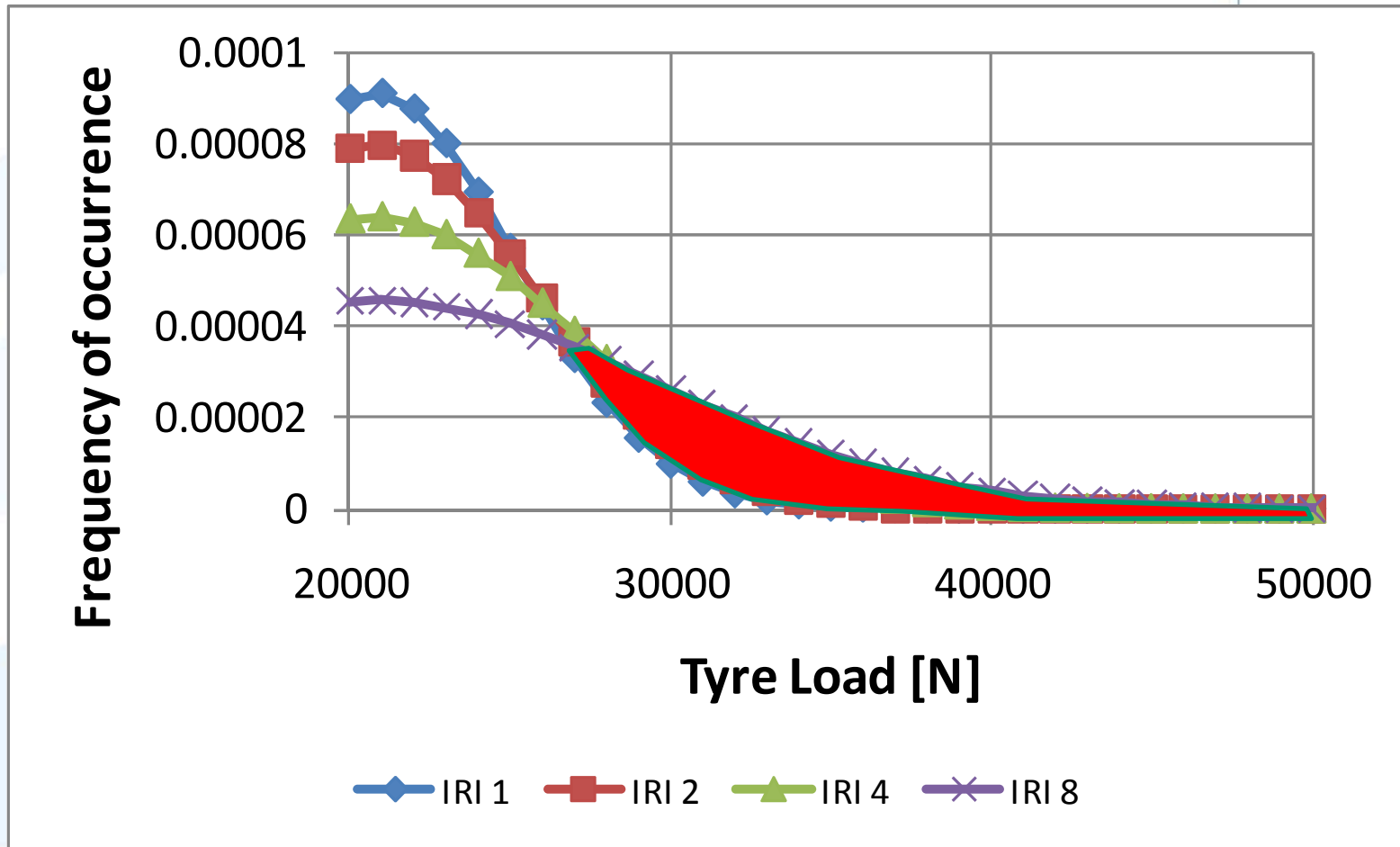
- Part of overall SANRAL project
- Focus on improved definition of the traffic loads
- Process
  - Simulate trucks on range of roads
  - Analyse outputs
  - Develop relationships
  - Apply in design and analysis
- Outside this presentation scope
  - WIM data, traffic counts, Tyre contact stresses







# Riding quality vs Tyre loads



# Simulation process

- Use TruckSIM
- Simulates vehicle travelling on pavement profile
- Well developed and calibrated



TruckSim Run Control: [ UC Caltrans ] Artic 710 nbl3\_2 empty 100km/h

File Edit Datasets Libraries Tools View Help

Run801 04-25-2010 01:20:08

Test Specifications

Vehicle configuration: S\_SS + SS

UC Caltrans artic basic empty

Procedure

US710 nbl3\_2 100 km/h

Run Control: Built-In Solvers

Run Math Model

Results (Post Process)

Animate

Rear View, Road Ref. w/o Yaw (Fit. Fa)

Plot

Simulation results (Exc)

TruckSim Mechanical Simulation

UC Caltrans artic basic empty (Tractor Trailers)

View

Vehicle: Lead Unit with 3 Axes: [ TS 3A Trucks ] 3A Tractor 5.5T/15.5T/15.5T (18 spd.)

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Lead3a101 12-16-2009 11:13:00

Vehicle configuration: 5.5T/15.5T/15.5T (18 spd.)

3A Sleeper Cab Sprung Mass

3A Sleeper

3300kg Steer, 3000kg Drive/1 andem

1/25 (Typical)

6x4, axes 2 & 3

330 kW, 18 spd. MT, 4WD

Static load for rear axle of: 0.5

Dynamic load transfer coefficient: 0.45

Load transfer due to brake torque: 0 1/m

Dist back: 5636 mm

Height: 1100 mm

Hitch

5th Wheel (Typical)

Animation Settings

Animator shape(s): Vehicle Shape

3A Sleeper

Steering wheel torque: 1/25 (Typical)

Powertrain: 6x4, axes 2 & 3

Tandem for axes 2 & 3

Static load for rear axle of: 0.5

Dynamic load transfer coefficient: 0.45

Load transfer due to brake torque: 0 1/m

Axle 1 X distance back: 0 mm

Axle 2 X distance back: 5000 mm

Axle 3 X distance back: 6270 mm

Susp Km: 5.5t Steer, Single Wheel - Kinematics

15.5t Drive, Dual Wheels - Kinematics

15.5t Drive, Dual Wheels - Kinematics

Comp: 5.5t Leaf: +150 mm, -60 mm Travel

15.5t Leaf: +100 mm, -60 mm Travel

15.5t Leaf: +100 mm, -60 mm Travel

Brakes: 7.5 kN-m Capacity, Air

10 kN-m Capacity, Air

10 kN-m Capacity, Air

Steering: Medium (5 m) Wheelbase

No Steering

No Steering

Misc.: Misc.

Misc.: Misc.

Misc.: Misc.

Vehicle: Lead Unit Spring Mass: [ Tractors ] 3A Sleeper Cab Spring Mass

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Spring182 06-21-2010 07:28:04

Height (for animation): 3200

Width (for animation): 5438

Lateral coordinate of mass center: B

Mass center of unladen sprung mass: 1015

Origin of spring mass coordinate system

All dimensions and coordinates are in millimeters

The inertial properties are for the spring mass in the design configuration, with no additional loading

Spring mass: 6308 kg

Roll inertia (Ixx): 6879 kg-m<sup>2</sup>

Pitch inertia (Iyy): 21711 kg-m<sup>2</sup>

Yaw inertia (Izz): 19685 kg-m<sup>2</sup>

Product (Ixy): 0 kg-m<sup>2</sup>

Product (Ixz): 130 kg-m<sup>2</sup>

Product (Iyz): 0 kg-m<sup>2</sup>

Roll radius of gyration: 83.1 in

Pitch radius of gyration: 146.5 in

Yaw radius of gyration: 139.8 in

Inertia and radius of gyration are related by the equation:  $I = MR^2$

Frame Torsional Flexibility

Check this box to use opto mode. The optional mode torsional flexibility of the LH and RH trailers, and a further suspended unit.

The extended models require

Vehicle: [ TS Traps ] 3000 kg Rating, 3.10 mm Radius

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Tire181 06-16-2010 11:04:16

Vertical Force

Use the force table

Vertical force: Tire Fz vs Deflection

800Pa HVIS type

Animator Settings

Tire width: 268 mm

The unloaded radius is also used to locate the animated wheel.

Use custom animator description:

Animator: Shape Group

Super Single w/ Brake

Animator: Sound Set

The Sounds

Dynamic Properties

Tire and wheel spin moment of inertia (added to the spin inertia of the unspinning)

14 kg-m<sup>2</sup>

Tire Lag

Tire force or moment

Distance rolled

L for Fx: 50 mm

L for Fy and Mz: 1000 mm

The models use modified equations to simulate the lag for Fy and Mz at speeds below this threshold.

Cut-off speed: 0 km/h

Rolling Resistance Moment Parameters

Rolling resistance coefficient: 0.008

Rolling resistance coefficient: 0.000256

Include rolling resistance due to Fx

Shear Forces and Moments

Longitudinal force: Tire Fx

Fx - 3000 kg Load Rated Tire

Lateral force: Tire Fy

Fy - 3000 kg Load Rated Tire

Aligning moment: Tire Mz

Mz - 3000 kg Load Rated Tire

Constant thrust

Constant Coefficient - B D1

Insulation (gamma)

Wheel plane

Wheel center

Wheel spin axis

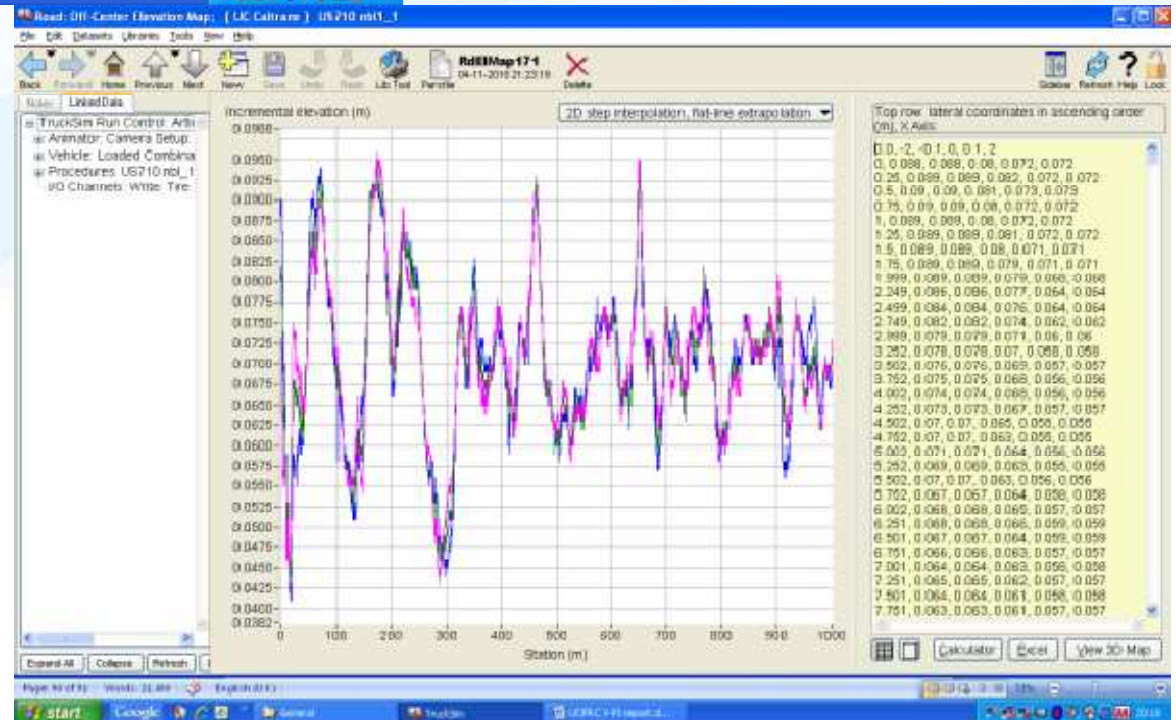
Center of Tire Contact (CTC)

Velocity of CTC

Fx, Mx

Fy, My

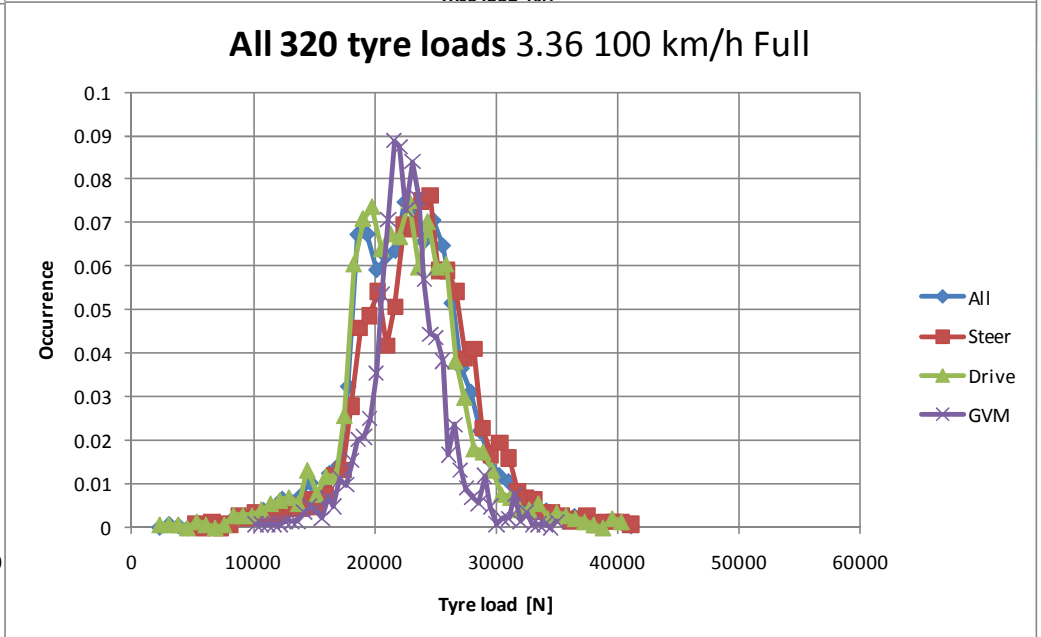
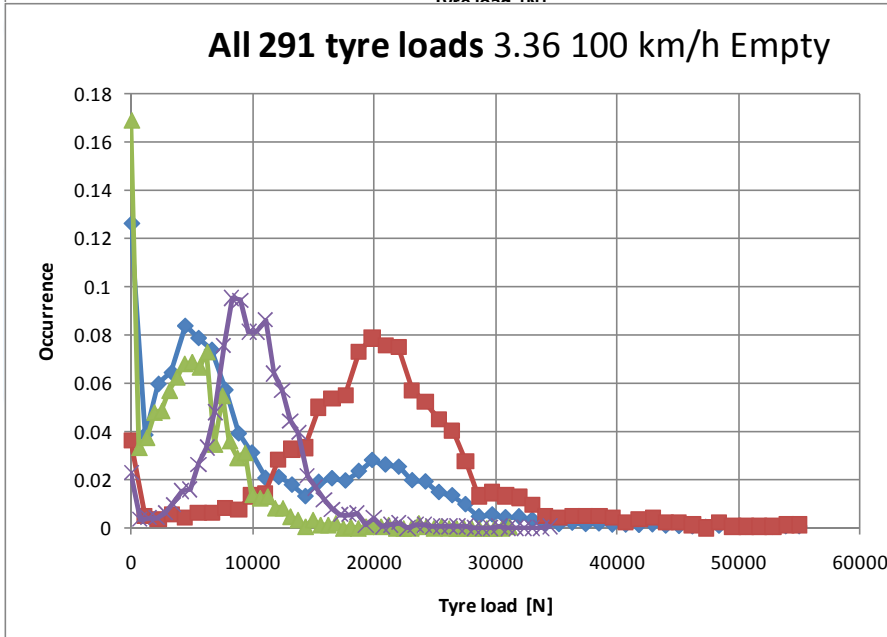
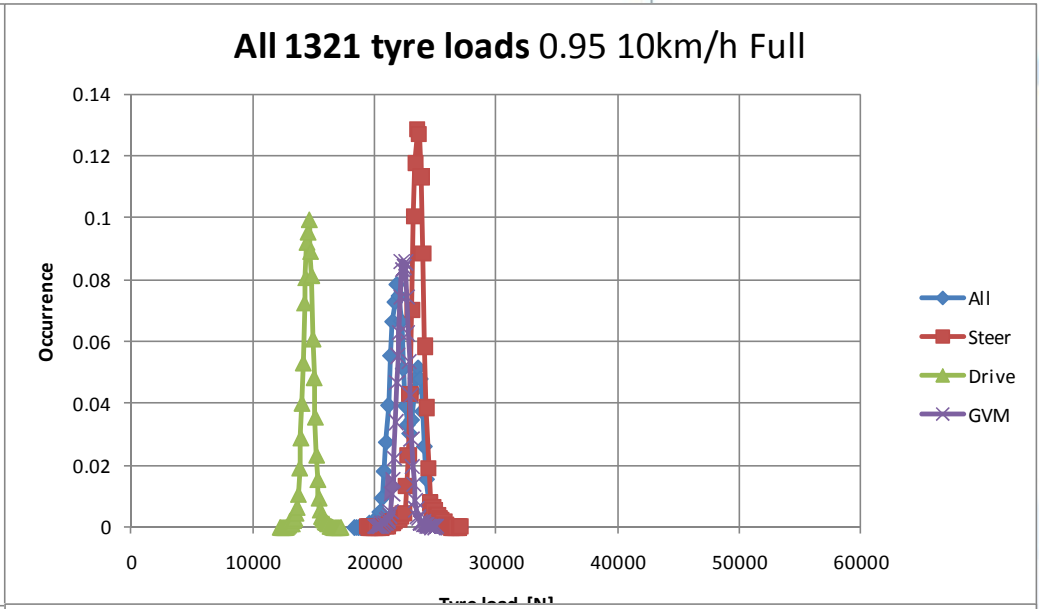
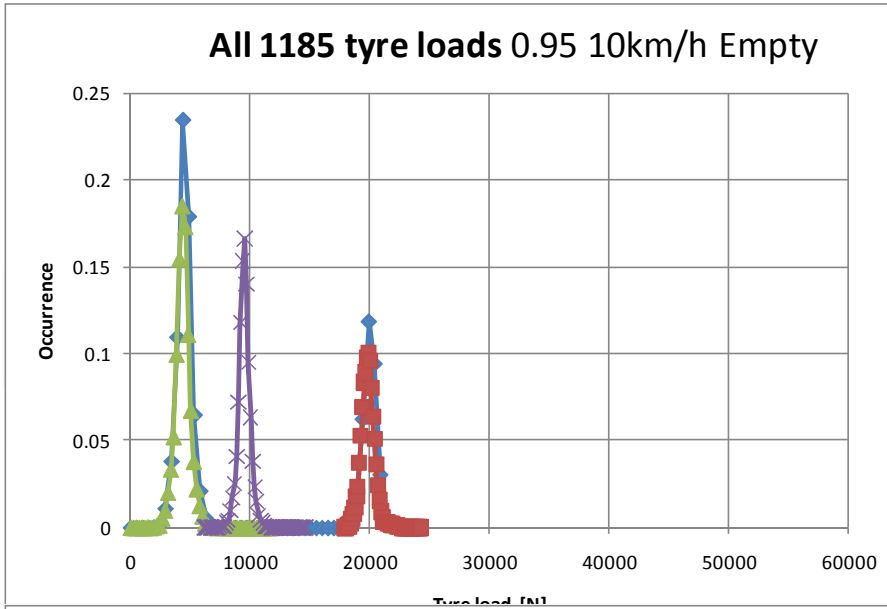
Fz, Mz



# Matrix

- Rigid, Articulated, Interlink
- Empty, full, 10% overloaded
- 10, 40, 80, 100 km/h
- IRI range – (0) 1.07 to 3.71 m/km

# Tyre load comparisons Rigid (axles converted to tyres)



# Initial relationships for Rigid

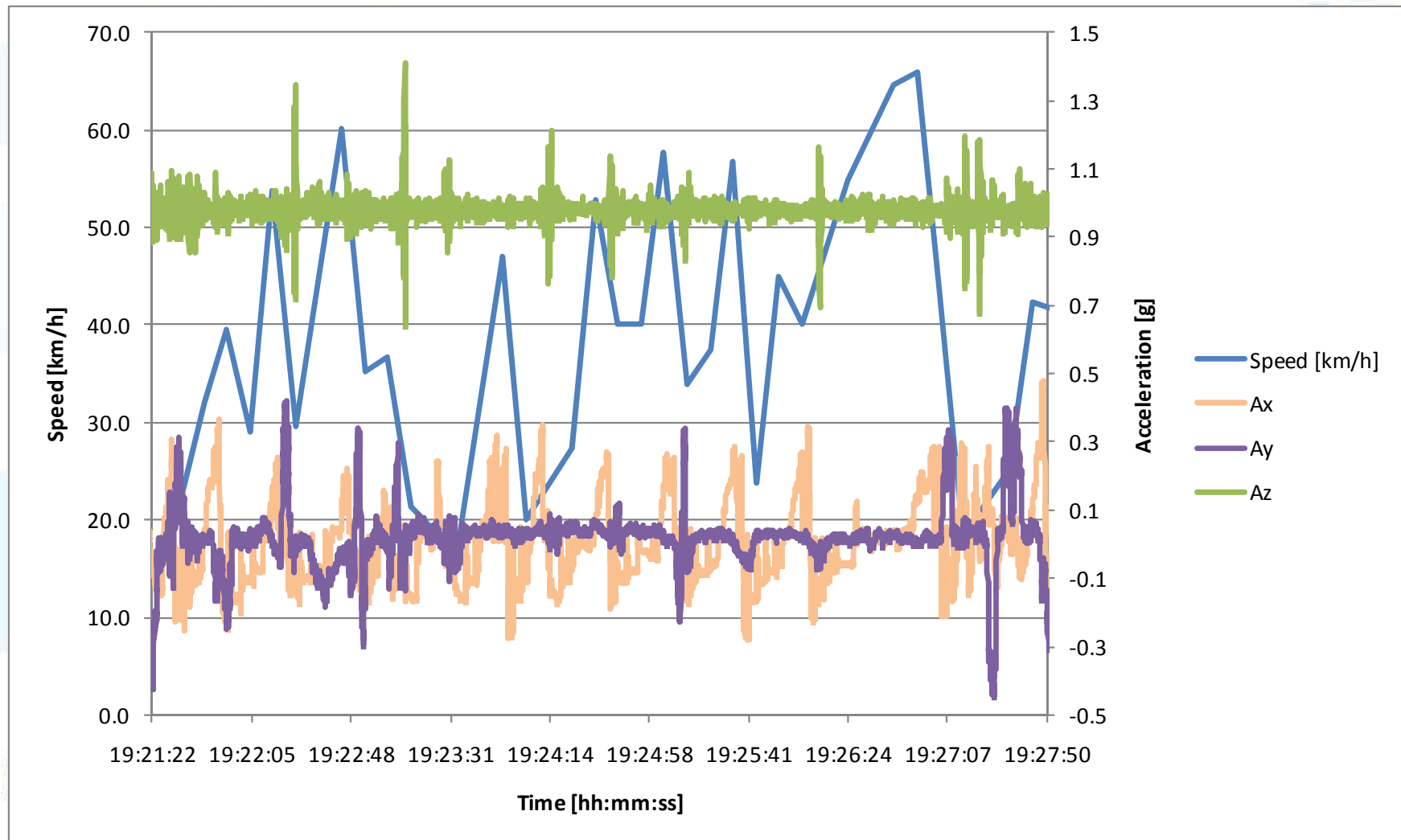
- Relationships for tyres, axles, axle groups, vehicles
- **CoV** =  $-0.0643 + 0.0198 \cdot \text{HRI} + 0.0058 \cdot \text{Speed} - 1.2152\text{E-}07 \cdot \text{GVM} - 5.2393\text{E-}07 \cdot \text{Load}$   
–  $R^2 = 98.6$  per cent; SE = 0.03
- **Ave** =  $36086.112 + 0.533 \cdot \text{HRI} - 101.623 \cdot \text{Speed} + 0.5210 \cdot \text{GVM/wheel} - 0.0221 \cdot \text{Load}$   
–  $R^2 = 99.7$  per cent; SE = 336.420

## Proposed process

- Measure actual traffic on a spot (WIM)
- Convert to static through WIM calibration
- Use as input together with speed, vehicle type, road roughness and relationships to predict expected MDL per axle type
- Select data from distribution for iterative Monte Carlo analysis in pavement design

# Cargo accelerations due to road profile

- State of Logistics issues



# Conclusions

- Riding quality of roads deteriorate with use leading to changes in road profile
- Increases in road roughness leads to increased dynamic loads and increased number of higher-than-average tyre loads
- Changing riding quality affects design and analysis loads over lifetime



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