



UNIVERSITEIT VAN PRETORIA
UNIVERSITY OF PRETORIA
YUNIBESITHI YA PRETORIA

AN IMPROVED TOOL FOR M-E EVALUATION OF PAVEMENT PERFORMANCE

Dr James W. Maina, PhD, Pr. Eng, F.SAICE, F.SAAE, M.SAT
Professor
Dept of Civil Engineering,
University of Pretoria, South Africa



Outline of the Presentation

Improving the numerical modelling for pavement analysis

1. Pavement (structural) performance
2. M-E evaluation of pavement performance
3. Loading cases
4. Materials models
5. Numerical integration and its challenges
6. Efforts to improve accuracy and speed
7. Some examples
8. Concluding Remarks



1. Pavement (structural) performance



Fatigue cracking and ageing

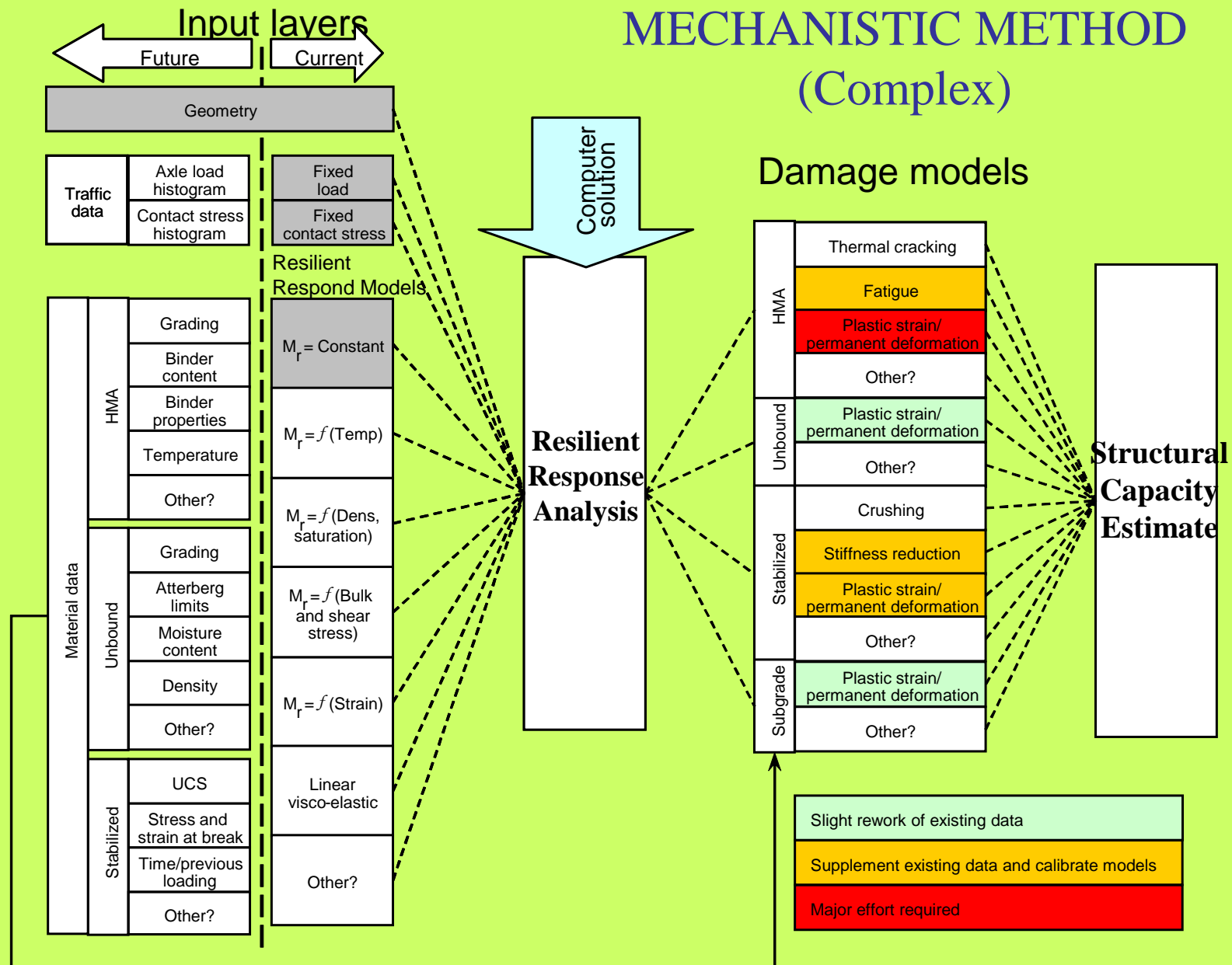


rutting – plastic deformation

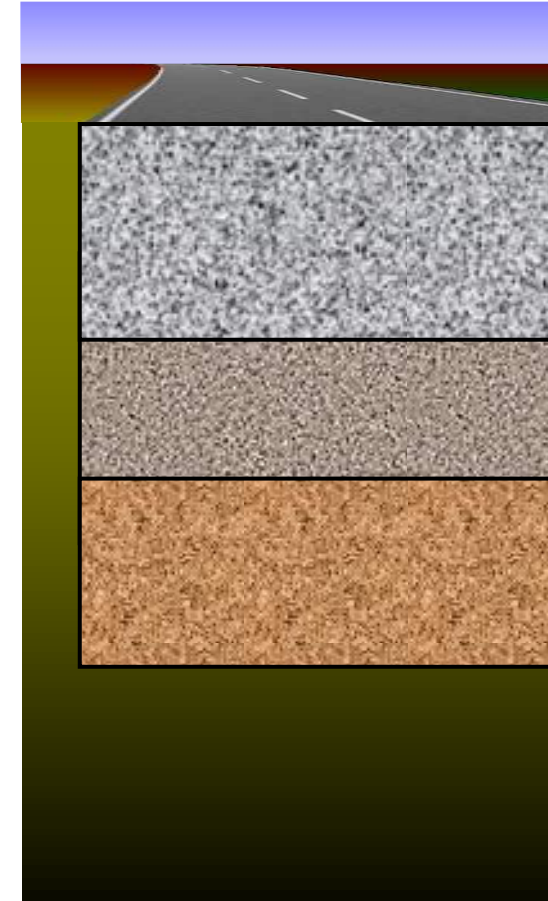
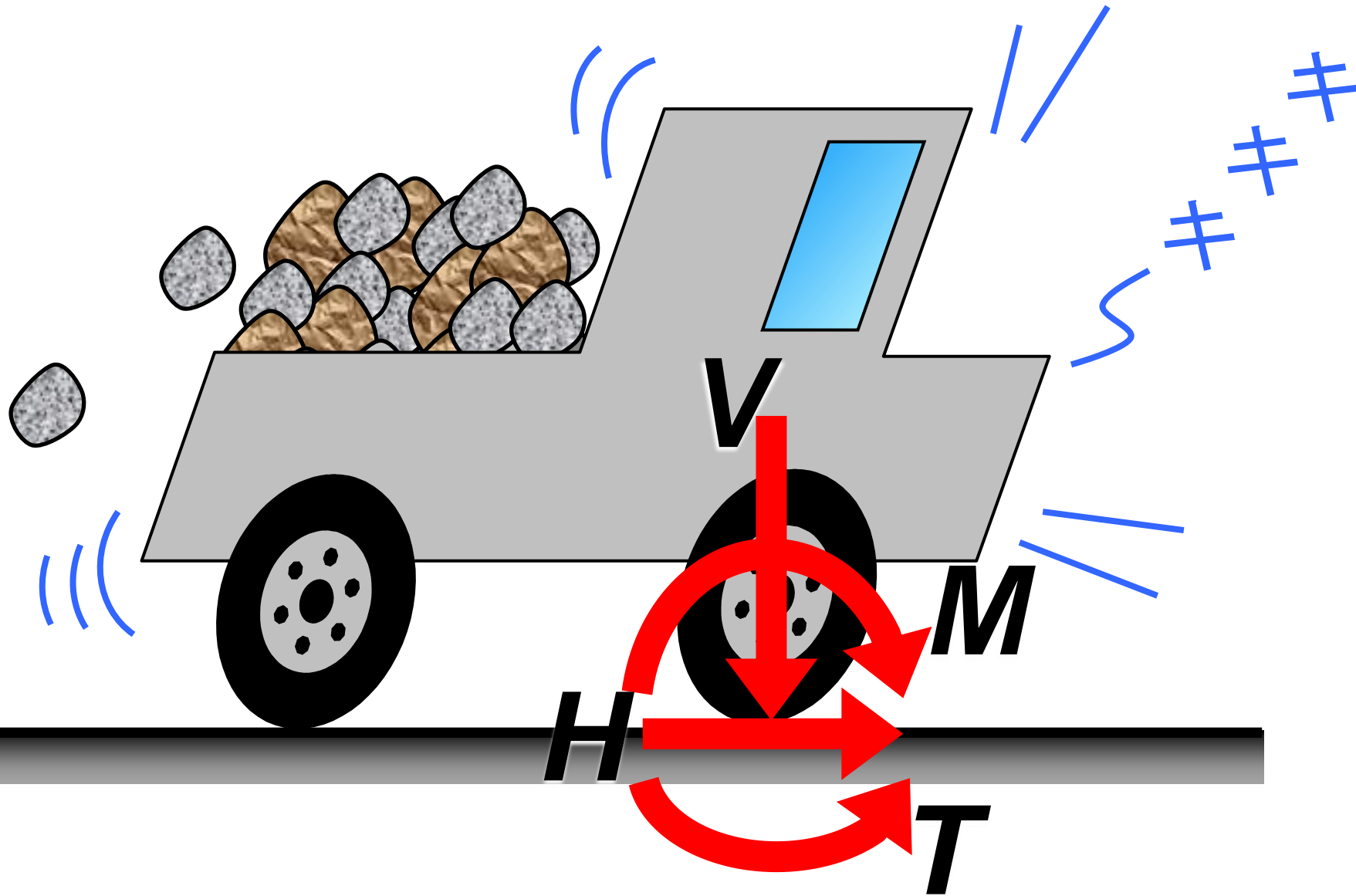


shoving – start and stop

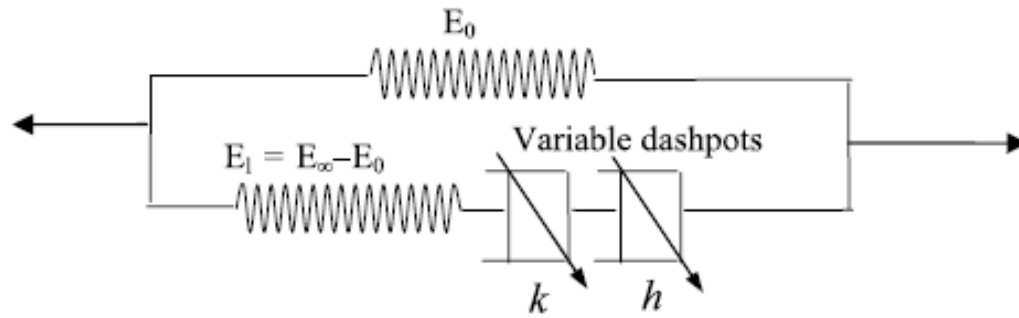
2. M-E Evaluation of Pavement Performance



3. Loading Cases

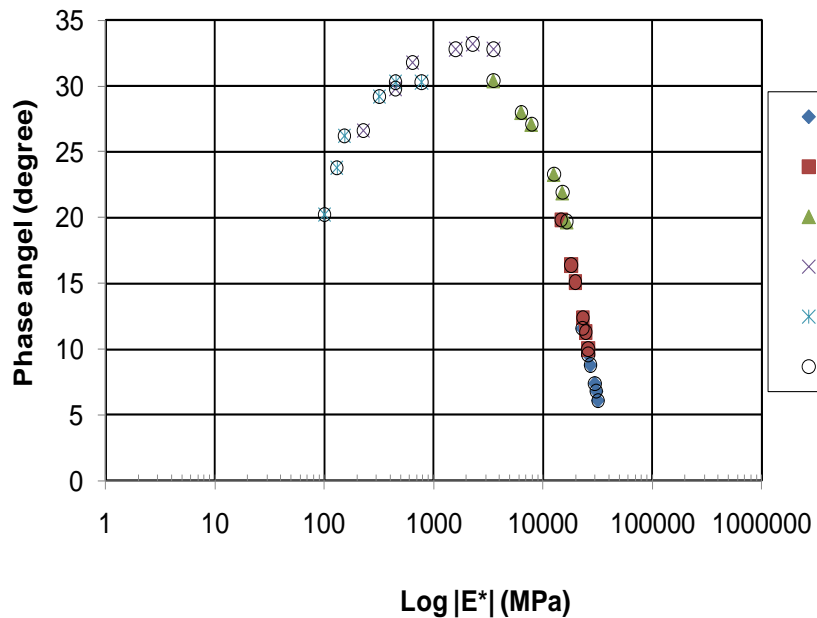


4. Materials models

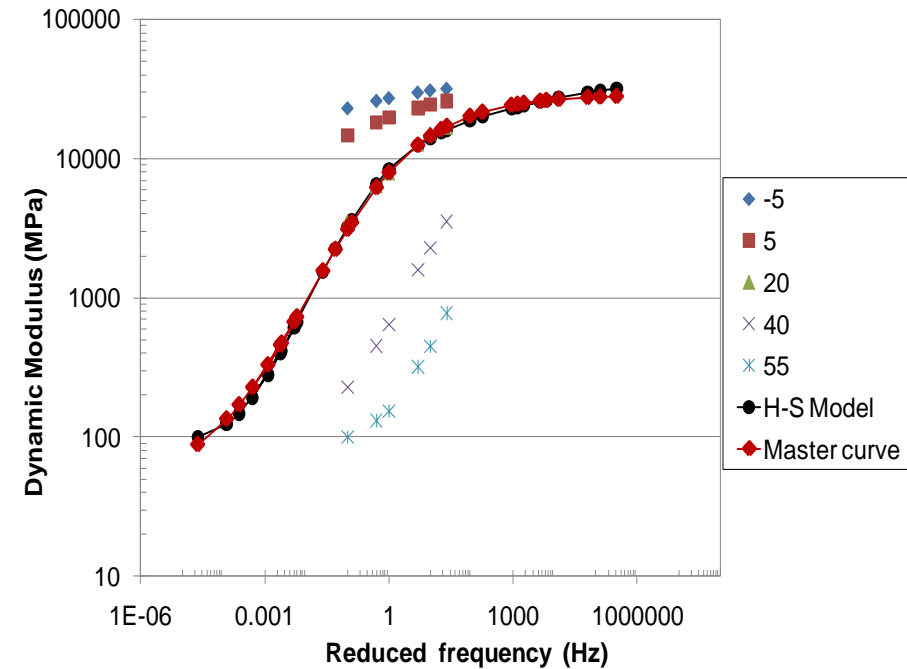
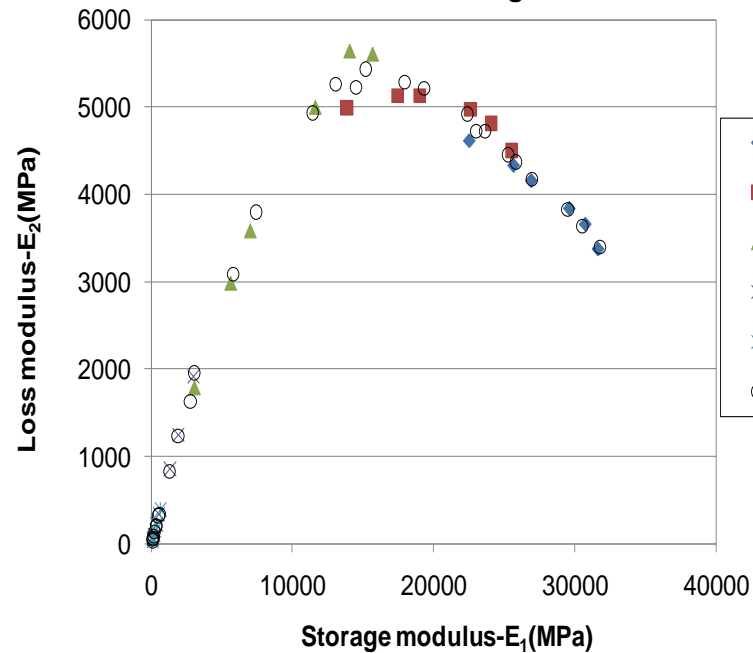


Huet-Sayegh Model

Black diagram



Cole-Cole diagram



4. Materials models

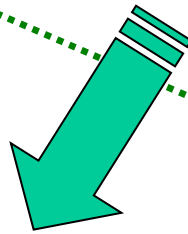
Isotropic material

E : constant elastic modulus

ν : constant Poisson's ratio

G : shear modulus

$$G = \frac{E}{2(1+\nu)}$$



Cross-anisotropic material

E_v : vertical elastic modulus

E_h : horizontal elastic modulus

G_{vh} : shear modulus

ν_v : vertical Poisson's ratio

ν_h : horizontal Poisson's ratio



5. Numerical Integration and its Challenges

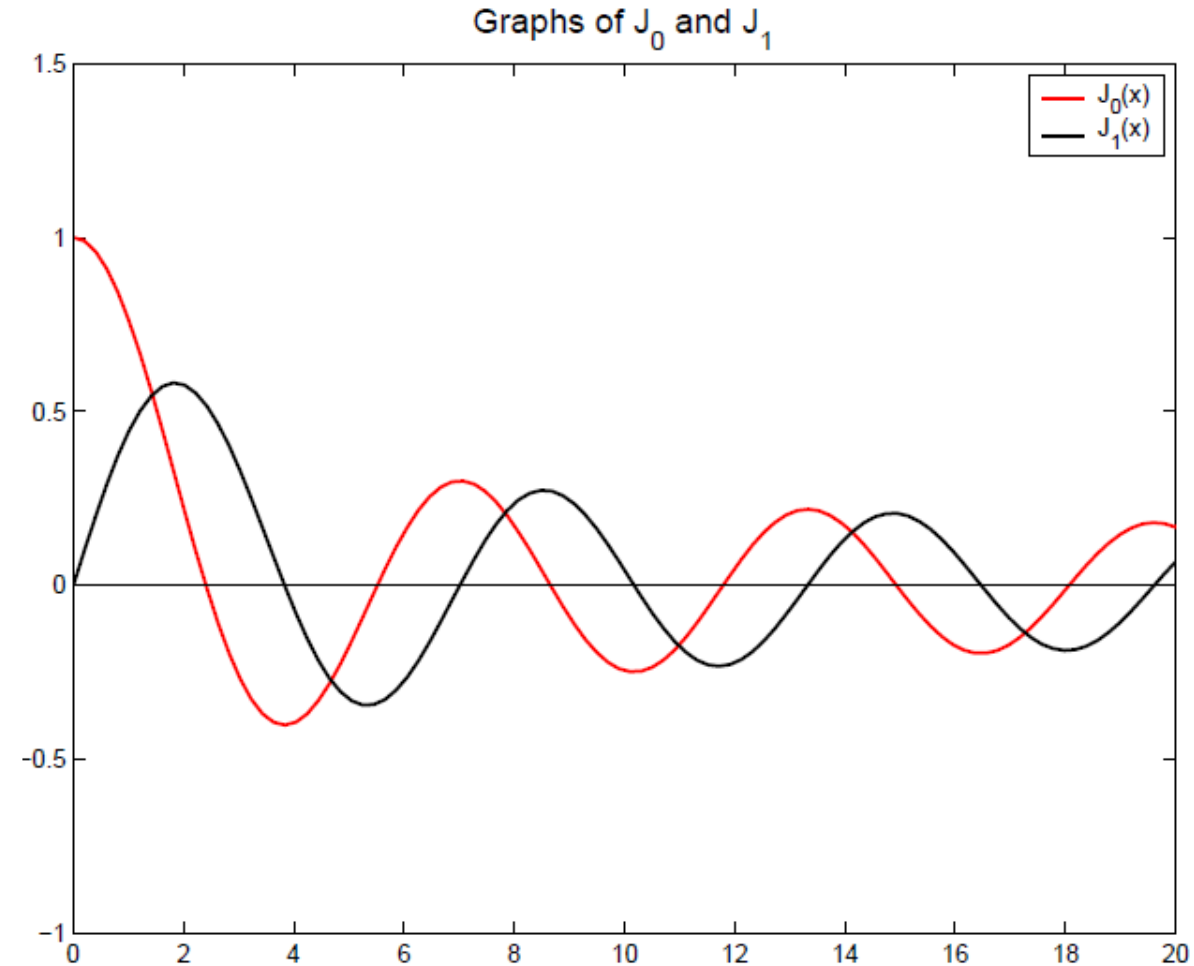
Hankel inverse transform of responses:

$$U_r = \int_0^{\infty} \xi \bar{U}_r J_1(\xi r) J_1(\xi a) d\xi$$

$$U_z = \int_0^{\infty} \xi \bar{U}_z J_0(\xi r) J_1(\xi a) d\xi$$

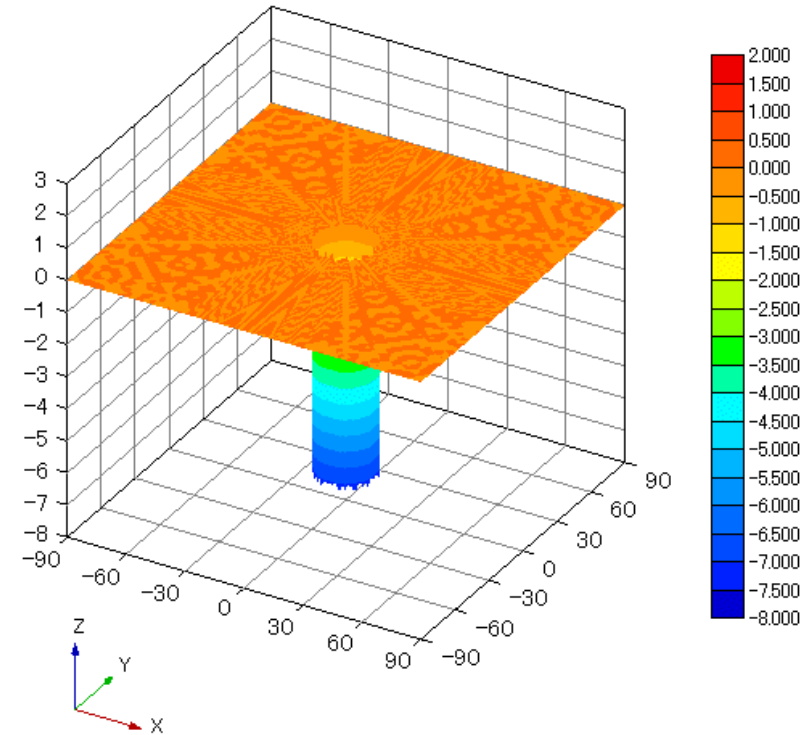
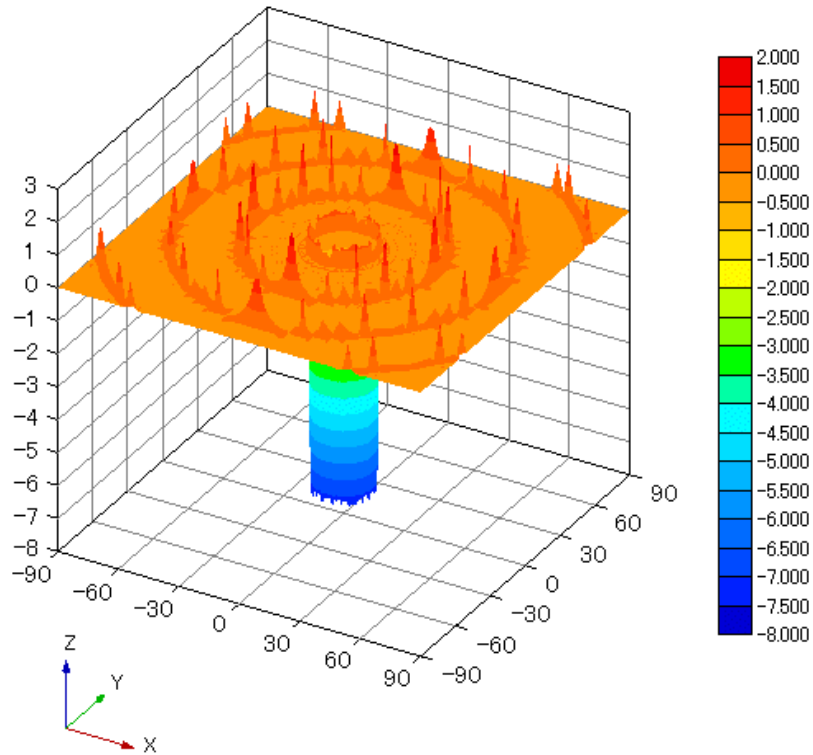
$$\sigma_z = \int_0^{\infty} \xi \bar{\sigma}_z J_0(\xi r) J_1(\xi a) d\xi$$

$$\tau_{rz} = \int_0^{\infty} \xi \bar{\tau}_{rz} J_1(\xi r) J_1(\xi a) d\xi$$



6. Efforts to improve speed and accuracy

3D plots of surface stress



Double Exponential (DE)
Transforms

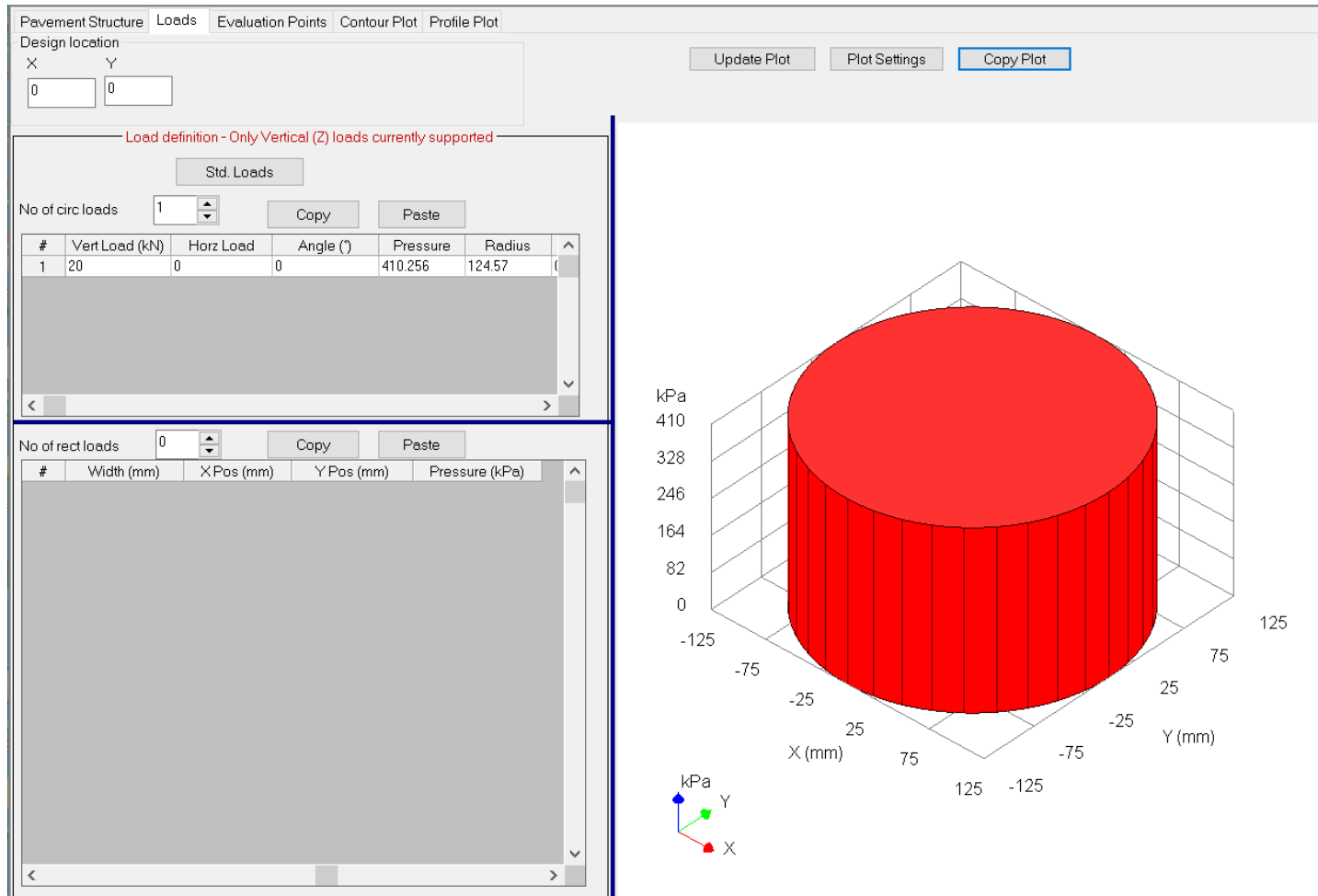
+

Richardson's extrapolation

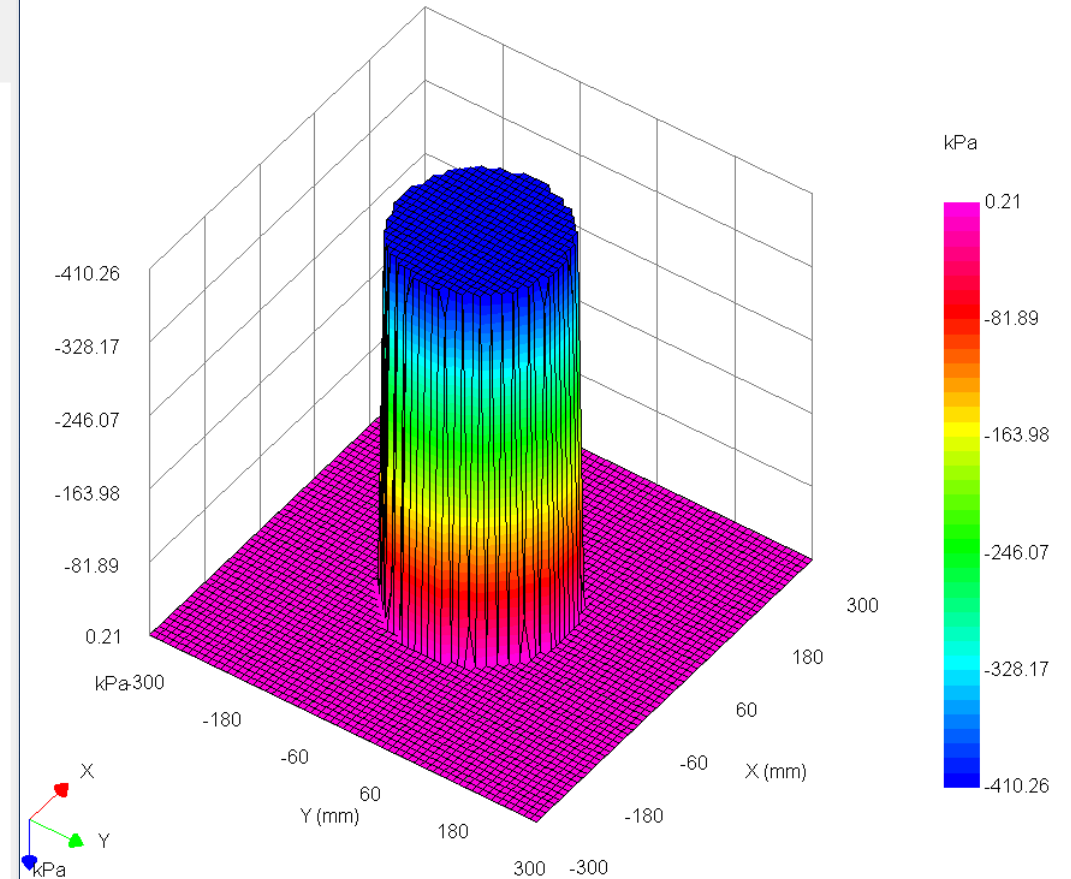
$$I = \lim_{\alpha \rightarrow 0} \int_0^{\infty} f(x) \exp(-ax^2) dx$$


6. Efforts to improve speed and accuracy

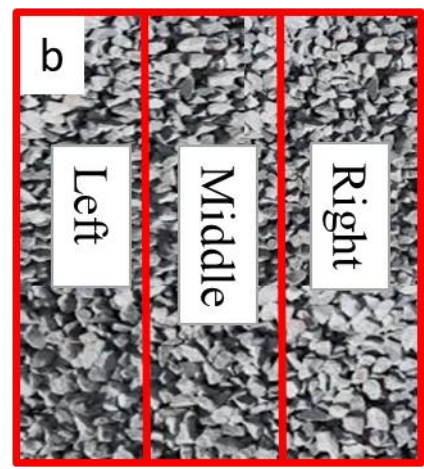
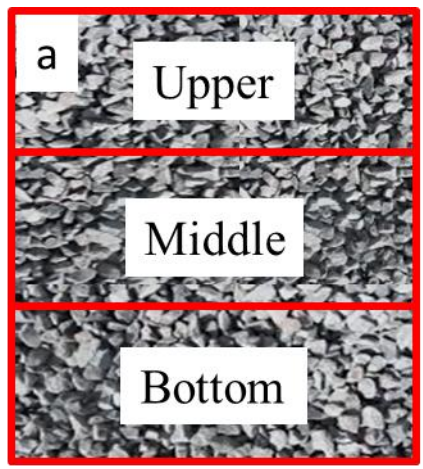
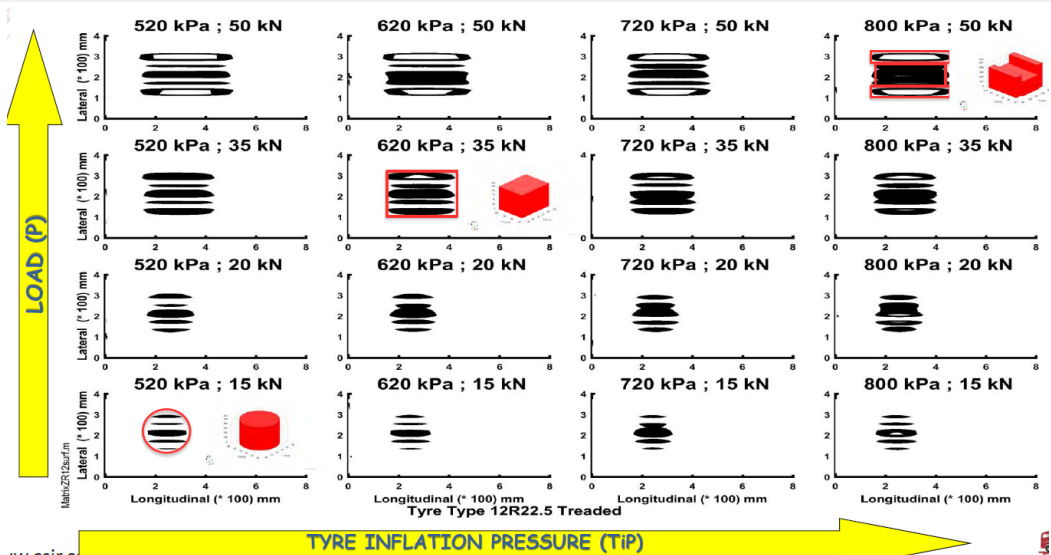
3D plots of surface stress



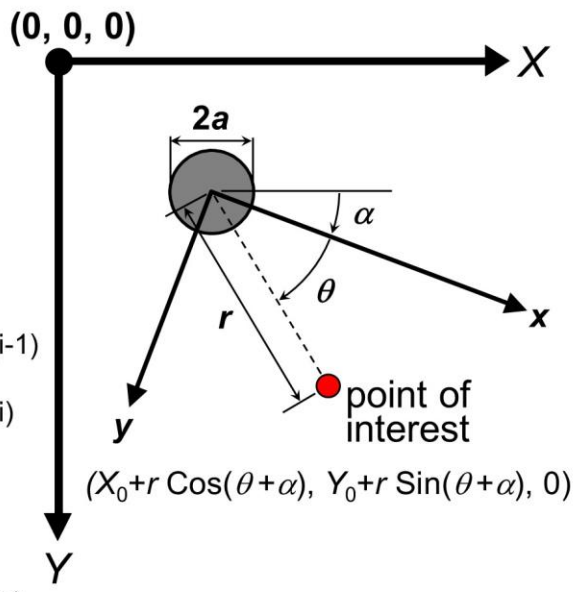
Horizontal plane parallel to X-Y at Z = 0 (Maximum 0.205556 at -250,-120)
Normal Stress ZZ



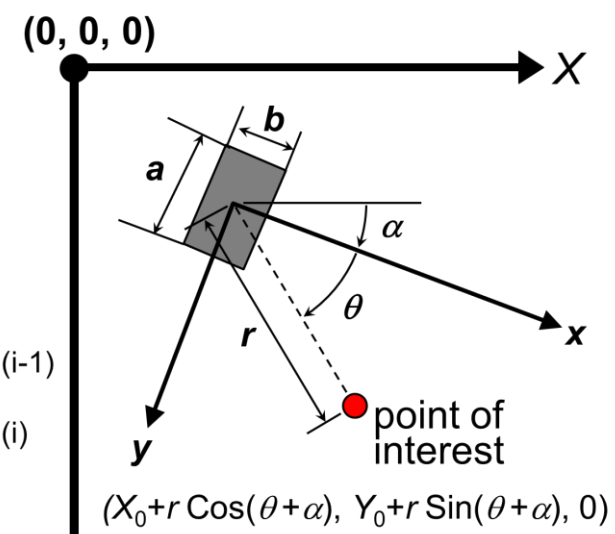
7. Some examples



Layer Thickness	Young's Modulus	Poisson's ratio
h_1	$E_{v1} E_{h1}$	$\nu_{v1} \nu_{h1}$
h_2	$E_{v2} E_{h2}$	$\nu_{v2} \nu_{h2}$
h_{i-1}	$E_{v(i-1)} E_{h(i-1)}$	$\nu_{v(i-1)} \nu_{h(i-1)}$
h_i	$E_{v(i)} E_{h(i)}$	$\nu_{v(i)} \nu_{h(i)}$
	$E_{v(n)} E_{h(n)}$	$\nu_{v(n)} \nu_{h(n)}$



Layer Thickness	Young's Modulus	Poisson's ratio
h_1	$E_{v1} E_{h1}$	$\nu_{v1} \nu_{h1}$
h_2	$E_{v2} E_{h2}$	$\nu_{v2} \nu_{h2}$
h_{i-1}	$E_{v(i-1)} E_{h(i-1)}$	$\nu_{v(i-1)} \nu_{h(i-1)}$
h_i	$E_{v(i)} E_{h(i)}$	$\nu_{v(i)} \nu_{h(i)}$
	$E_{v(n)} E_{h(n)}$	$\nu_{v(n)} \nu_{h(n)}$



7. Some examples

Pavement Structure | Loads | Evaluation Points | Design Parameters | Pavement Life | Contour Plot | Profile Plot | Calculation Table

Number of Layers: 3 | Number of Phases: 1 | Default input: On | Cross-anisotropy: On | Copy | Paste

#	Material	Thickness	E-modulus	E-modulus	Poisson's	Poisson's	Slip Rate	Density	Saturation
	Phase 1	(mm)	Ev (MPa)	Eh (MPa)	Muz (MPa)	Muh (MPa)	0-0.99	82-89 %	3-89 %
1	AC	150	5000	5000	0.44	0.44	0		
2	G2	150	450	450	0.35	0.35	0	86	30
3	Subgrade	0	100	100	0.35	0.35	0		

Pavement Structure | Loads | Evaluation Points | Design Parameters | Pavement Life | Contour Plot | Profile Plot | Calculation Table

Number of Layers: 3 | Number of Phases: 1 | Default input: On | Cross-anisotropy: On | Copy | Paste

#	Material	Thickness	E-modulus	E-modulus	Poisson's	Poisson's	Slip Rate	Density	Saturation
	Phase 1	(mm)	Ev (MPa)	Eh (MPa)	Muz (MPa)	Muh (MPa)	0-0.99	82-89 %	3-89 %
1	AC	150	5000	5000	0.44	0.44	0		
2	G2	150	450	250	0.35	0.35	0	86	30
3	Subgrade	0	100	100	0.35	0.35	0		



7. Some examples

Transfer functions for HMA surfacing layers

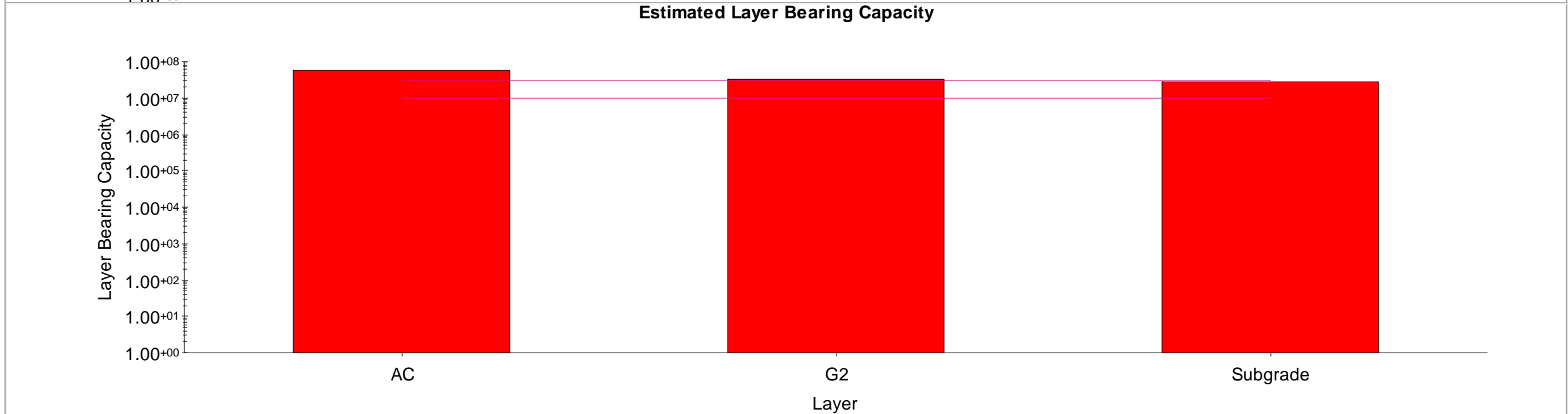
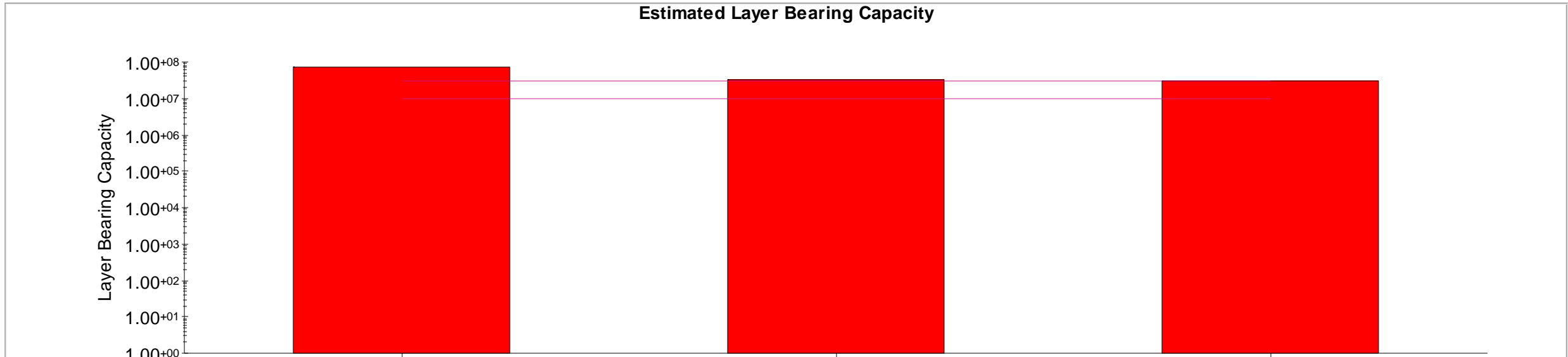
$\log N_f = I - S (\log \epsilon_t) - offset$

Material code	Intercept	Slope	Offsets			
			50%	80%	90%	95%
AC	18.114	5.195	0	0.242	0.352	0.469
AG	17.725	4.774	0	0.382	0.425	0.437

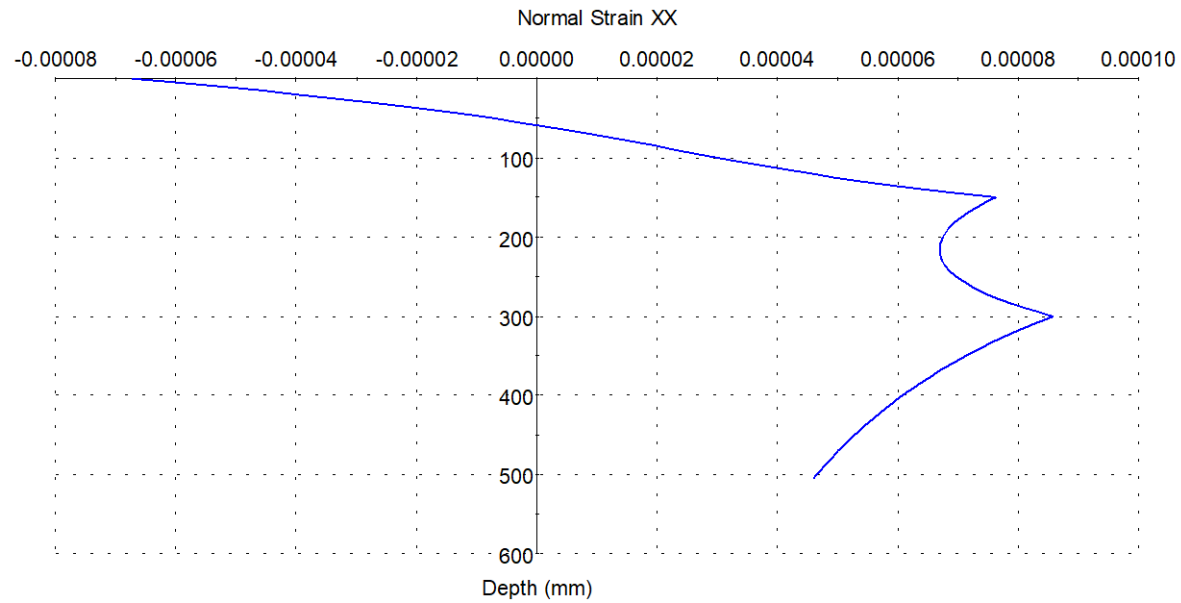
Reset OK Cancel Help



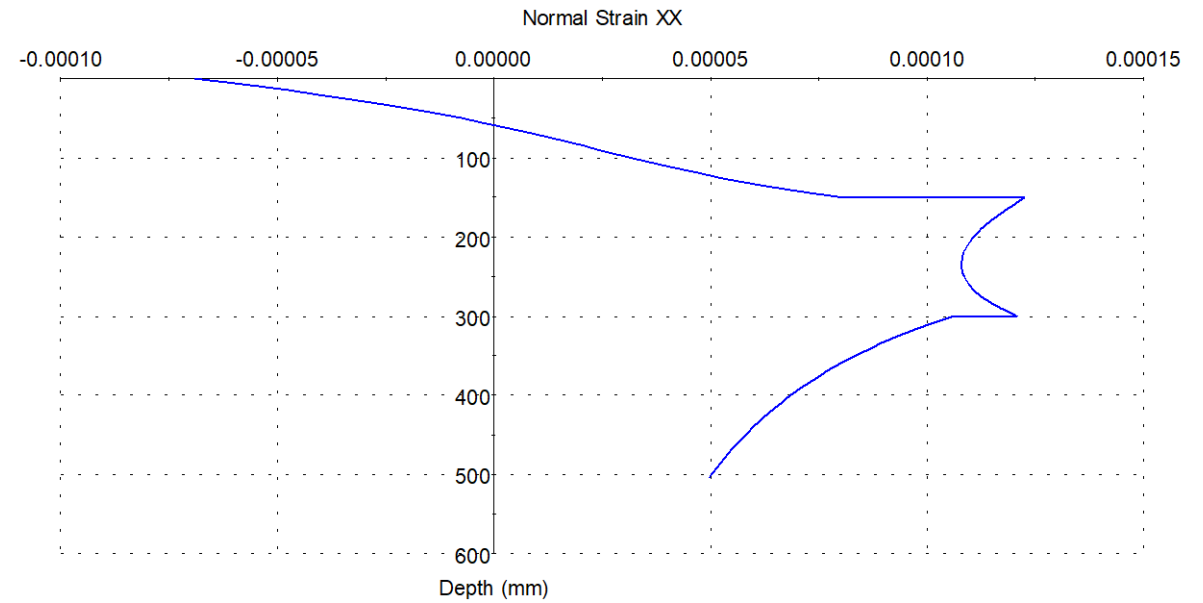
7. Some examples



7. Some examples



Isotropic base-layer



Transversely-Isotropic base-layer



8. CONCLUDING REMARKS

- ▶ A partnership between industry and academia/research council is important
- ▶ Information from the laboratories and field are important for realistic numerical modelling of pavement structures
- ▶ Computation power is available at reasonable cost for realistic pavement modelling and analysis
- ▶ With the support from industry, academia/research council have the skills and capability to develop user friendly and powerful tools for M-E pavement design and analysis.

